

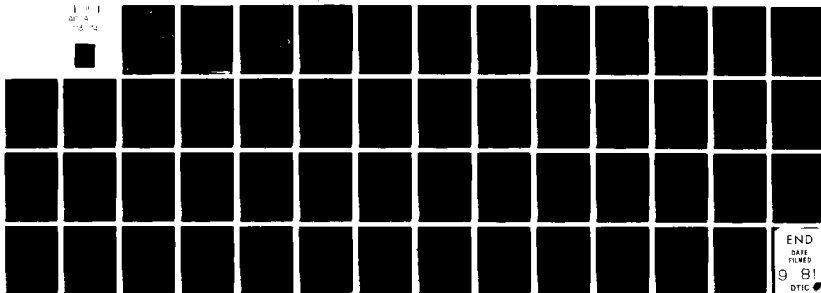
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DEVELOPMENT AND APPLICATION OF A SUBSONIC TRIANGULAR VORTEX PAN--ETC(U)
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DEVELOPMENT AND APPLICATION OF A SUBSONIC TRIANGULAR VORTEX PANEL

John C. Sparks

Loads and Dynamics Branch
Structures Division

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February 1981

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FOREWORD

This report was prepared by Mr. John C. Sparks of the Loads and Dynamics Branch (ENFSL), Structures Division (ENFS), Aeronautical Systems Division (ASD), Wright-Patterson Air Force Base, Ohio. The work was accomplished to help fulfill the requirements for the degree of Master of Science at the Air Force Institute of Technology. Appreciation is extended to my advisor, Major Stephen J. Koob of the Department of Aeronautics and Astronautics, Air Force Institute of Technology and to James R. Snyder of ASD/XRHI for his valuable suggestions. Appreciation is also extended to Capt. Ron Luther who found a programming error in the original computer code. The elimination of this error vindicated the theory and made this report possible.

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List of Symbols

Symbol

αangle of attack
$\vec{\omega}$vorticity vector
$\delta(x,y), \gamma(x,y), 0$Components of $\vec{\omega}$
A, B, Ccoefficients of the assumed "bilinear" form for γ
D, E, Fcoefficients of the assumed "bilinear" form for δ
x_i, y_ipanel corner points
δ_i, γ_icorner vorticity values
x, y, zchordwise, spanwise, and normal coordinates, respectively
Γstraight line segment
\vec{s}control point in the plane $z = 0$
u, v, wperturbation velocities in the respective x, y, and z directions
$\vec{i}, \vec{j}, \vec{k}$unit vectors in the respective x, y, and z directions
Rregion of integration
Mnumber of chordwise panels or slope (Appendix A only)
Nnumber of spanwise panels
\wedgeleading edge slope (Section III)
(θ_j)column vector of corner vorticities
(A_{ij})coefficient matrix premultiplying (θ_j)
M_∞free stream Mach number
V_∞free stream velocity

List of Symbols

Symbol

 dc/dx

.....camber slope

 γ

.....ratio of specific heats (eqs 3.30 and 3.31 only)

 $f_i(x, y)$

.....integrands obtained through application of the Biot-Savart Law

 F_i

.....improper integrals of the form

$$\lim_{L \rightarrow \infty} \int_{y_0}^{y_1} \int_{(y-b)/M}^L f_i(x, y) dx dy \quad i = 1, \dots, 5$$

 S_i

.....strip function

 I_i

.....integral over a triangular region

 C_p

.....pressure coefficient

 C_L

.....local lift coefficient

 C_M

.....local pitching moment coefficient

Subscripts and Superscripts

L

.....leading triangle

T

.....trailing triangle

ABSTRACT

Paneling methods are approximate techniques for solving flow problems over wings and bodies. Vortex panels are used to model flow over wings and other lifting surfaces. The author develops a triangular vortex panel having a vorticity distribution that can vary in magnitude and direction. This panel is used to predict the pressure distribution on a rectangular and a sweptback wing in subsonic flow. Lift distributions obtained compare favorably to Anderson's solution and wind tunnel results.

DEVELOPMENT AND APPLICATION
OF A SUBSONIC TRIANGULAR
VORTEX PANEL

I. Introduction

Background

Paneling methods are approximate techniques for solving linearized subsonic and supersonic potential flow problems over wings and bodies. Panels in use today incorporate singularity distributions of the source, vortex, and doublet types. Source panels are often used to model bodies and other non-lifting surfaces and to model thickness of lifting surfaces. Vortex panels are used to model either lifting or non-lifting surfaces. In a typical problem, the airplane is represented by a finite number of panels. Each panel is a singularity distribution of unknown strength that models some part of the aerodynamic surface. These unknown strengths are determined by applying the flow tangency boundary conditions at or near the aerodynamic surfaces. Once the strengths are known, the perturbation velocities can be computed. These are substituted into the Bernoulli equation to obtain the pressure distribution and the corresponding aerodynamic forces and moments.

Problem Statement

In many current paneling methods, the orientation of the vorticity vector is fixed on the panel (Ref 6 and Ref 8). This leads to unacceptable errors in some cases. The purpose of this study is to

derive a subsonic triangular panel having a vorticity distribution that can vary both in magnitude and direction. A panel system is assembled and used to predict the pressure distribution on a planform. Since the computations involved are too lengthy to be performed by hand, a computer code was developed to apply the panels to planar wings.

Approach

The subsonic triangular panel is derived in Section II. The Biot-Savart Law is used to compute the induced velocity at a point due to an assumed bilinear vorticity distribution on the panel. This expression formulates the induced velocity in terms of panel geometry and unknown corner point vorticity.

Section III presents methodology for panel system assembly. Numbering schemes are developed for panels and the unknown corner point vorticities. Planform boundary conditions are applied which reduce the number of unknowns and the remaining unknowns are solved for by formulating a linear system of equations. This system consists of control point equations (one per panel) and a number of edge continuity conditions. The linearized form of the flow tangency boundary condition is then used to effect the solution. Once the corner vorticities are known, the vorticity at any point on the planform can be obtained. Finally, induced velocities and corresponding pressures can be calculated from the known vorticity.

Section IV presents program predictions for a rectangular wing

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which are compared against Anderson's solution (Ref 1:9-16). Predictions are also presented for a swept untapered wing which are compared against wind tunnel tests (Ref 4:92).

Section V concludes the report and makes recommendations for the improvement of the aerodynamic model.

11. Panel Derivation

This section presents the development of the subsonic triangular panel. The goal is to derive an expression for the induced velocity at an arbitrarily chosen point in the xy plane due to an assumed bilinear vorticity distribution on the panel.

Geometry

The first step in panel development is the definition of panel geometry. Initially assume the panel is a trapezoid lying in the xy-plane and having two edges parallel to the x-axis. It is then subdivided into two triangles having a common side that joints the upper left hand corner to the lower right hand corner. The panel is oriented so that the root and tip chords lie parallel to the free stream flow direction at $\alpha = 0$. Figure 1 depicts the panel geometry, corner point numbering scheme, and coordinate system.

Singularity Strength Distribution

The general form of the singularity strength distribution on the panel will be

$$\vec{\omega}(x, y) = \delta(x, y)\vec{i} + \gamma(x, y)\vec{j} \quad (2.1)$$

where δ and γ are continuous functions of x and y. For the purpose of this study, δ and γ are assumed to have the "bilinear" forms

$$\delta(x, y) = F + Dx + Ey \quad (2.2)$$

$$\gamma(x, y) = A + Bx + Cy \quad (2.3)$$

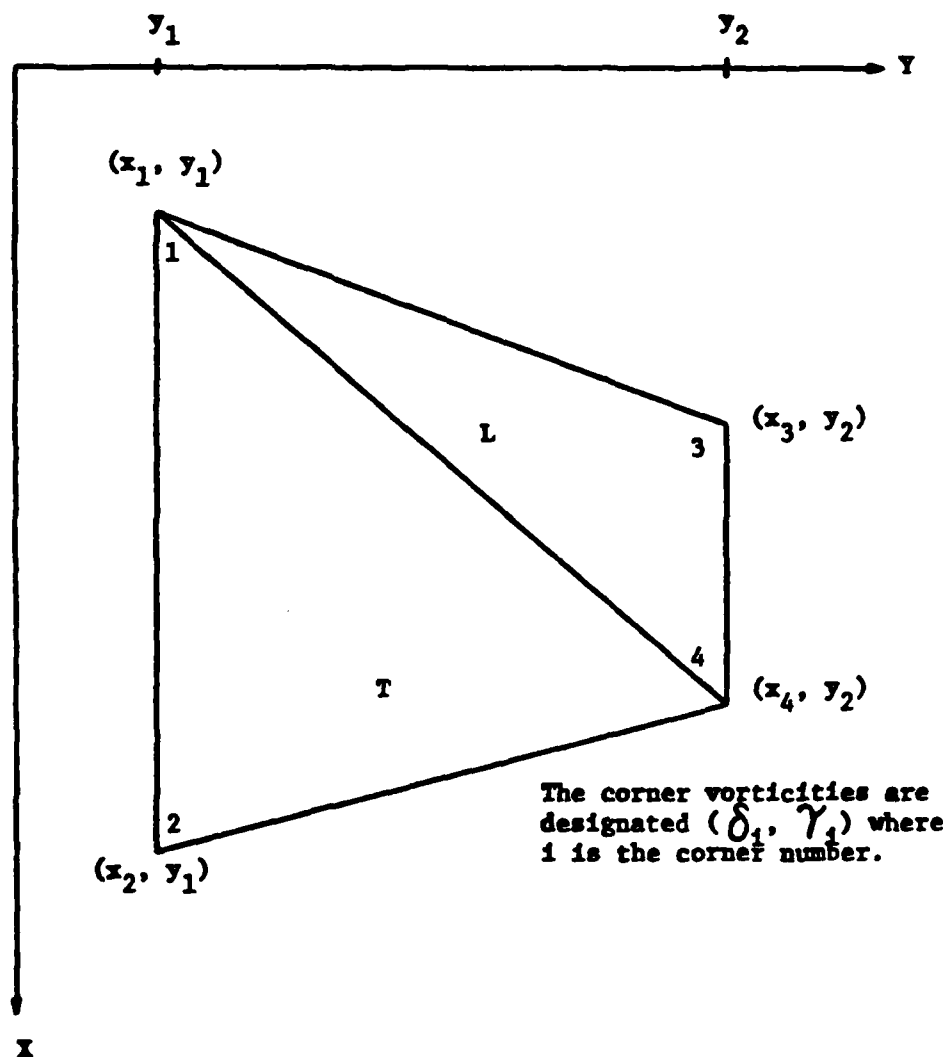


Figure 1. Panel Geometry and Corner Point Numbering Scheme

where the coefficients A, B, C, D, F, D and E are yet to be determined constants. These constants will be expressed as functions of the panel geometry and the unknown singularity strengths at the corner points.

Consequence of the Helmholtz Condition

The vorticity distribution $\vec{\omega}(x, y)$ is required to satisfy the Helmholtz condition that vorticity must be preserved in the fluid. Thus,

$$\nabla(\delta_j + \gamma_j) = 0 \quad (2.4)$$

on the panel. If δ and γ have the forms (2.2) and (2.3), respectively, then

$$\partial(F + Dx + Ey)/\partial x + \partial(A + Bx + Cy)/\partial y = 0 \quad (2.5)$$

which implies

$$D = -C \quad (2.6)$$

such that

$$\delta(x, y) = F - Cx + Ey \quad (2.7)$$

The formulation could be continued in terms of the bilinear coefficients. However, it is conventional to express them in terms of panel corner point vorticities.

Bilinear Coefficients in Terms of Corner Vorticity

In the ensuing discussion, the subscript L refers to the leading triangle and the subscript T refers to the trailing triangle.

The γ component of vorticity (eq (2.3)) is assigned the unknown values $\gamma_1, \gamma_3, \gamma_4$ at the corners (x_1, y_1) , (x_3, y_2) , and (x_4, y_2) of the leading triangle. This leads to the following system of three

equations in A_L , B_L and C_L :

$$\gamma_1 = A_L + B_L x_1 + C_L y_1 \quad (2.8)$$

$$\gamma_3 = A_L + B_L x_3 + C_L y_2 \quad (2.9)$$

$$\gamma_4 = A_L + B_L x_4 + C_L y_2 \quad (2.10)$$

The system has the solution:

$$A_L = y_2 \gamma_1 / (y_2 - y_1) + [(y_1 x_4 - x_1 y_2) / (y_2 - y_1)]$$

$$\gamma_3 / (x_3 - x_4) + [(x_1 y_2 - y_1 x_3) / (y_2 - y_1)]$$

$$\gamma_4 / (x_3 - x_4) \quad (2.11)$$

$$B_L = (\gamma_3 - \gamma_4) / (x_3 - x_4) \quad (2.12)$$

$$C_L = -\gamma_1 / (y_2 - y_1) + [(x_1 - x_4) / (y_2 - y_1)] \gamma_3 /$$

$$(x_3 - x_4) + [(x_3 - x_1) / (y_2 - y_1)] \gamma_4 /$$

$$(x_3 - x_4) \quad (2.13)$$

Since $D_L = -C_L$, only two corner conditions may be used to solve for F_L and E_L in the δ component eq (2.7). Assigning the values δ_1 and δ_3 at the corners (x_1, y_1) and (x_3, y_2) leads to

$$\delta_1 + C_L x_1 = E_L y_1 + F_L \quad (2.14)$$

$$\delta_3 + C_L x_3 = E_L y_2 + F_L \quad (2.15)$$

and

$$E_L = (\delta_1 - \delta_3)/(y_1 - y_2) + [(x_1 - x_3)/(y_1 - y_2)]c_L \quad (2.16)$$

$$F_L = (y_1 \delta_3 - y_2 \delta_1)/(y_1 - y_2) + [(y_1 x_3 - x_1 y_2)/(y_1 - y_2)]c_L \quad (2.17)$$

In a similar way, the trailing triangle coefficient equations are obtained as follows:

$$A_T = y_1 \gamma_4/(y_1 - y_2) + [(y_2 x_1 - x_4 y_1)/(y_1 - y_2)] \gamma_2/(x_2 - x_1) + [(x_4 y_1 - y_2 x_2)] \gamma_1/(x_2 - x_1) \quad (2.18)$$

$$B_T = (\gamma_2 - \gamma_1)/(x_2 - x_1) \quad (2.19)$$

$$C_T = -\gamma_4/(y_1 - y_2) + [(x_4 - x_1)/(y_1 - y_2)] \gamma_2/(x_2 - x_1) + [(x_2 - x_4)/(y_1 - y_2)] \gamma_1/(x_2 - x_1) \quad (2.20)$$

$$E_T = (\delta_2 - \delta_4)/(y_1 - y_2) + [(x_2 - x_4)/(y_1 - y_2)]c_T \quad (2.21)$$

$$F_T = (y_1 \delta_4 - y_2 \delta_2)/(y_1 - y_2) + [(y_1 x_4 - x_2 y_2)/(y_1 - y_2)]c_T \quad (2.22)$$

where E_T and F_T have been expressed in terms of (as functions of) $\bar{\omega}$ components at corners 2 and 4.

Mathematical Continuity

The bilinear vorticity distribution is continuous on each triangular region. In addition, the γ component has been made to be continuous throughout the planform by the representation in terms of corner values. This can be demonstrated as follows. Let Γ be the boundary shared by any two adjacent triangles. Then Γ is a straight line segment and can be described by a linear expression (i.e., y in terms of x or x in terms of y). The γ distribution on each of the adjacent triangles will degenerate to a linear function of a single variable upon substitution of this expression. Both functions assume the same γ values at the endpoints of Γ . Since only two points are needed to determine a straight line or a linear form, we have γ matching identically on Γ .

The δ component has breaks in continuity throughout the planform. This is a consequence of applying the Helmholtz condition (eq (2.4)) which eliminated the constant D and expressing the remaining two unknowns in terms of two δ corner values, out of a possible three. The δ component is continuous on panel leading and trailing edges since it is on these edges that common δ values are assumed at the endpoints. The δ component is discontinuous on panel diagonals.

Application of the Biot-Savart Law

Let $\bar{\omega}(\hat{x})$ be a vorticity distribution defined on a finite region R in the xy plane. Let ξ be a fixed point (control point) in the plane.

The velocity induced at \vec{s} due to the distribution on R is given by the Biot-Savart Law (Ref 5:526-528):

$$4\pi\vec{v}(\vec{s}) = \iint_R [\vec{\omega}(\vec{x}) \times (\vec{s} - \vec{x})] / |\vec{s} - \vec{x}|^3 dR \quad (2.23)$$

Suppose the control point \vec{s} is located at the origin of the coordinate system. Note that this can be done by performing a simple translation of the plane. Then,

$$\vec{s} = (0, 0, 0) \quad (2.24)$$

$$\vec{s} - \vec{x} = (0, 0, 0) - (x, y, 0) = (-x, -y, 0) \quad (2.25)$$

Assuming the distribution has the form (2.1),

$$\vec{\omega} \times (\vec{s} - \vec{x}) = [x\gamma - y\delta] \vec{k} \quad (2.26)$$

where \vec{k} is the unit vector normal to the xy-plane. Substituting the expressions (2.25) and (2.26) into eq (2.23) yields:

$$4\pi w(0, 0, 0) = \iint_R (x\gamma - y\delta) / (x^2 + y^2)^{3/2} dR \quad (2.27)$$

Where w is the normal velocity component induced at the origin.

Substituting the expressions for γ (2.3) and δ (2.7) into eq (2.27) yields:

$$4\pi w = \iint_R (Ax + Bx^2 + 2Cxy - Ey^2 - Fy) / (x^2 + y^2)^{3/2} dR \quad (2.28)$$

where R is taken as the region defined by a trapezoidal panel.

Let R_L and R_T be the subregions of R which correspond to the lead-

ing and trailing triangles. The coefficients A, B, C, F, and E remain constant on each subregion and eq (2.28) is rewritten as:

$$4\pi w = A_L I_1^L + A_T I_1^T + B_L I_2^L + B_T I_2^T + 2C_L I_3^L + 2C_T I_3^T - F_L I_4^L - F_T I_4^T - E_L I_5^L - E_T I_5^T \quad (2.29)$$

where

$$I_3^{L, T} = \iint_{R_{L, T}} (x/(x^2 + y^2)^{3/2}) dR \quad (2.30)$$

$$I_2^{L, T} = \iint_{R_{L, T}} (x^2/(x^2 + y^2)^{3/2}) dR \quad (2.31)$$

$$I_3^{L, T} = \iint_{R_{L, T}} (xy/(x^2 + y^2)^{3/2}) dR \quad (2.32)$$

$$I_4^{L, T} = \iint_{R_{L, T}} (y/(x^2 + y^2)^{3/2}) dR \quad (2.33)$$

$$I_5^{L, T} = \iint_{R_{L, T}} (y^2/(x^2 + y^2)^{3/2}) dR \quad (2.36)$$

Evaluation of these integrals may be found in Appendix A. Substitution of the expressions for A_L through E_T and collecting coefficients of the unknowns ($\delta_1, \delta_2, \delta_3, \delta_4, \gamma_1, \gamma_2, \gamma_3$, and γ_4) yields, after considerable algebraic manipulation,

$$\begin{aligned}
4 \pi w = & [(y_2^L - I_3^L)/(y_1 - y_2)] \delta_1 + \\
& [(y_2^T - I_5^T)/(y_1 - y_2)] \delta_2 + \\
& [(I_5^L - y_1 I_4^L)/(y_1 - y_2)] \delta_3 + \\
& [(I_5^T - y_1 I_4^T)/(y_1 - y_2)] \delta_4 + \\
& [((x_4 y_1 - y_2 x_2) I_1^T - (x_2 - x_1) y_2 I_1^L - \\
& (y_1 - y_2) I_2^T + (x_2 - x_1) K_L + \\
& (x_2 - x_4) K_T)/((x_2 - x_1)(y_1 - y_2))] \gamma_1 + \\
& [((y_2 x_1 - x_4 y_1) I_1^T + (y_1 - y_2) I_2^T + \\
& (x_4 - x_1) K_T)/((y_1 - y_2)(x_2 - x_1))] \gamma_2 + \\
& [((y_1 x_4 - x_1 y_2) I_1^L + (y_2 - y_1) I_2^L + \\
& (x_1 - x_4) K_L)/((y_2 - y_1)(x_3 - x_4))] \gamma_3 + \\
& [((x_1 y_2 - y_1 x_3) I_1^L - (x_3 - x_4) y_1 I_1^T - \\
& (y_2 - y_1) I_2^L + (x_3 - x_1) K_L + (x_3 - x_4) K_T)/ \\
& ((y_2 - y_1)(x_3 - x_4))] \gamma_4
\end{aligned} \tag{2.35}$$

where

$$\begin{aligned} \kappa_L = & 2I_3^L - [(x_1 - x_3)/(y_1 - y_2)]I_5^L - \\ & [(y_1x_3 - x_1y_2)/(y_1 - y_2)]I_4^L \end{aligned} \quad (2.36)$$

$$\begin{aligned} \kappa_T = & 2I_3^T - [(x_2 - x_4)/(y_1 - y_2)]I_5^T - \\ & [(y_1x_4 - x_2y_2)/(y_1 - y_2)]I_4^T \end{aligned} \quad (2.37)$$

Summary

Expression (2.35) is the normal velocity induced at the origin of the xy plane by a trapezoidal vorticity panel. This velocity is due to a bilinear vorticity distribution which satisfies the Helmholtz condition eq (2.4).

III. Panel Assembly

This section presents the panel assembly procedures needed to model a wing. The goal is to develop the methodology required to predict the pressure distribution and associated forces and moments on a wing.

Panel Numbering

Figure 2 illustrates a paneling arrangement and associated numbering scheme for a 16 panel wing. The panels are numbered consecutively in the chordwise direction starting with the inboard leading edge panels and terminating with the outboard trailing edge panels.

Number of Unknowns, Boundary Conditions and Numbering

Let M be the number of chordwise panels and N be the number of spanwise panels. These are defined using $M + 1$ chordwise cuts and $N + 1$ spanwise cuts. Each intersection determines a panel corner point. Since there are two unknown components at each corner point, the total number of unknowns is given by:

$$2(M + 1)(N + 1) \quad (3.1)$$

Boundary Conditions

Two boundary conditions are imposed on the wing panel system. These reduce the number of unknowns and improve the physical modeling of the flow field.

The Kutta condition (Ref 5:390-399)

The z axis is normal to the wing planform.

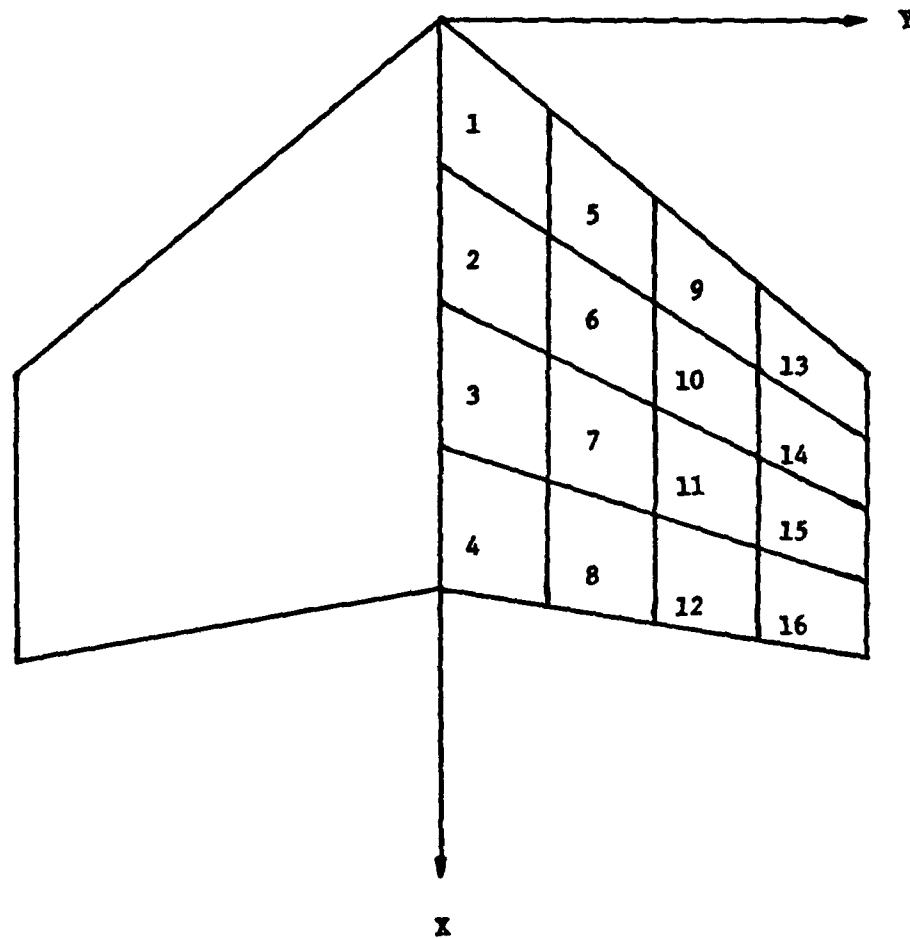


Figure 2. A Paneling Arrangement and Associated Numbering Scheme for a 16 Panel Wing

$$\gamma(x, y) = 0 \quad (3.2)$$

is imposed at all corner points on the wing trailing and tip edges. Since the γ component of vorticity eq (2.2) is both linear and continuous on these edges, the Kutta condition is satisfied identically. The Kutta condition reduces the total number of unknowns by:

$$M + N + 1 \quad (3.3)$$

(NOTE: The point defining the intersection of the trailing and tip edges is common to both.)

A historically acceptable boundary condition (an outgrowth of Prandtl's lifting-line theory (Ref 5:535-567)) is for the vorticity vector to lie tangent to the wing leading edge. This boundary condition initially orients the vorticity vector so that a positive circulation is produced. The boundary condition is imposed at all leading edge corner points and can be written:

$$\gamma/\delta = \Lambda \quad (3.4)$$

or

$$\delta = \gamma/\Lambda \quad (3.5)$$

where Λ is the leading edge slope at the corner point. It reduces the total number of unknowns by:

$$N + 1 \quad (3.6)$$

and the total number of unknowns becomes:

$$2MN + M \quad (3.7)$$

after imposing the two boundary condition equations (3.2) and (3.5).

Since the wing is symmetric about the x-axis, it may seem logical to impose a boundary condition at the wing root chord. However, setting

$$\delta = 0 \quad (3.8)$$

at the centerline is redundant for rectangular wings and leads to an ill-conditioned system once planform symmetry is considered.

Unknown Numbering Scheme

Figure 3 illustrates the unknown numbering scheme for a 9 panel wing with applied boundary conditions. The paneling arrangement of Figure 3 is chosen because it represents the smallest number of panels needed to illustrate interior panels and panels having boundary conditions. Let i be the panel number of an interior panel. Then the following numbers (in terms of i , M , and N) are assigned to the eight unknown corner vorticity components:

$$(\delta_1) \quad 1 - 1 \quad (3.9)$$

$$(\delta_2) \quad 1 \quad (3.10)$$

$$(\delta_3) \quad 1 + M - 1 \quad (3.11)$$

$$(\delta_4) \quad 1 + M \quad (3.12)$$

The unknown corner δ s are denoted by "-" and the γ s by "=".

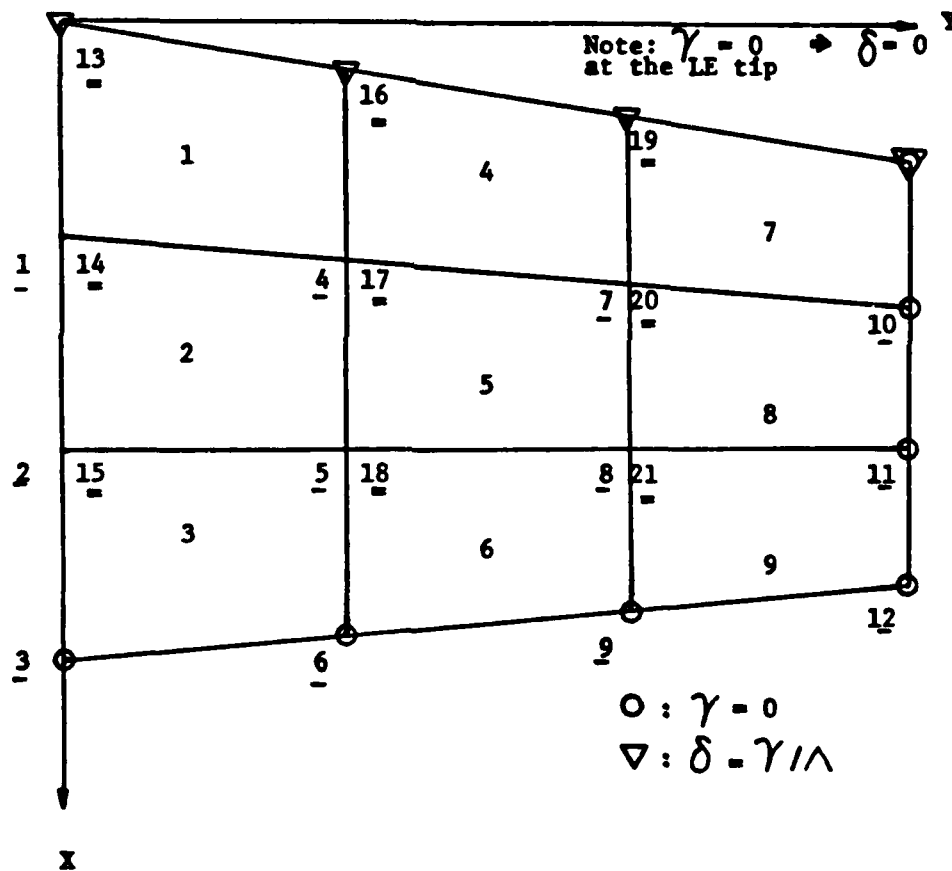


Figure 3. Unknown Numbering Scheme for a 9 Panel Wing

$$(\gamma_1) \quad MN + M + 1 \quad (3.13)$$

$$(\gamma_2) \quad MN + M + 1 + 1 \quad (3.14)$$

$$(\gamma_3) \quad MN + 2M + 1 \quad (3.15)$$

$$(\gamma_4) \quad MN + 2M + 1 + 1 \quad (3.16)$$

Solving for the Corner Vorticities

The total number of unknowns (after the boundary conditions are applied) is given by eq (3.7) which also specifies the number of conditions needed to solve for the corner vorticities. Two types of conditions will be used; control point conditions and edge or point continuity conditions.

Control Point Equations

Control point equations are obtained using eq (2.35). The velocity component is computed for one point (control point) on each panel comprising the wing.

Let (x_i, y_i) be the control point on panel i . To obtain the contribution to w_i due to panel j , express the coordinates of panel j in a coordinate system with (x_i, y_i) at the origin. This is done by performing a translation in the $z = 0$ plane:

$$\begin{aligned} x' &= x - x_i \\ y' &= y - y_i \end{aligned} \quad (3.17)$$

Equation (2.35) is then applied with appropriate boundary conditions.

Planform symmetry is included by reflecting either the panel or control point about the x-axis and applying eq (2.35). Reflecting the control point is less complicated from a programming viewpoint.

The above process is repeated for each panel on the wing. After all the contributions to w_i have been calculated, it can be written as:

$$w_i = \sum_{j=1}^{2MN+M} A_{ij} \theta_j \quad (3.18)$$

where θ_j is the column vector of unknown corner vorticities and the coefficients A_{ij} are functions of panel geometry. The θ_j are numbered using the system given by eqs (3.9) through (3.16). One control point equation (3.18) is obtained for each panel on the wing and together they comprise MN conditions.

Edge Continuity Conditions

The δ component of vorticity eq (2.7) is discontinuous across the panel diagonal (See discussion in Section II.). This can be partially remedied by specifying a point continuity condition at the panel lower right hand corner. This condition is:

$$\delta_L(x_4, y_2) = \delta_4 \quad (3.19)$$

which becomes

$$\begin{aligned} &\delta_4 - \delta_3 + [(x_3 - x_4)/(y_2 - y_1)] \gamma_1 - \\ &[(x_1 - x_4)/(y_2 - y_1)] \gamma_3 - [(x_3 - x_1)/ \\ &(y_2 - y_1)] \gamma_4 = 0 \end{aligned} \quad (3.20)$$

after substituting of (x_4, y_2) and the expressions for C_L (2.13), E_L (2.16), and F_L (2.17) into eq (2.7). One condition eq (3.20) is formulated for each panel on the wing for a total of MN condition. Note that δ is still not continuous across the panel diagonal due to the remaining discontinuity at the upper left hand corner. Also δ is not continuous across panel side edges.

The edge continuity conditions and control point equations total 2MN conditions. M additional conditions can be obtained by specifying an edge continuity condition for δ at the upper left hand corner of each panel along the centerline. This condition is

$$\delta_T(x_1, y_1) = \delta_1 \quad (3.21)$$

which becomes

$$\begin{aligned} \delta_2 - \delta_1 - [(x_2 - x_1)/(y_1 - y_2)] \gamma_4 + \\ [(x_4 - x_1)/(y_1 - y_2)] \gamma_2 + [(x_2 - x_4)/ \\ (y_1 - y_2)] \gamma_1 = 0 \end{aligned} \quad (3.22)$$

after substitution of (x_1, y_1) and the expressions for C_T (2.20), E_T (2.21), and F_T (2.22) into eq (2.7). This choice is based on trial and error, the additional δ continuity on the centerline having the effect of minimizing vorticity oscillations.

Compressibility

Compressibility effects are accounted for by using the Prandtl-Glauert transformation (Ref 2:124-127):

$$\bar{x} = x / \sqrt{1 - M^2} \quad (3.23)$$

The transformation is applied to all x coordinates which are used in either the control point equations or edge continuity conditions.

Matrix Formulation

The control point equations and edge continuity conditions are $2MN + M$ equations in the unknowns, θ_j . This system has the matrix formulation:

$$\begin{matrix} \left[A_{ij} \right] & \cdot & \begin{bmatrix} \theta_1 \\ \vdots \\ \theta_{2MN+M} \end{bmatrix} & = & \begin{bmatrix} w_1 \\ \vdots \\ w_{MN} \\ 0 \end{bmatrix} \\ (2MN+M) \times (2MN+M) & & & & \end{matrix} \quad (3.24)$$

The first MN rows of A_{ij} are the coefficients for the control point equations and are all nonzero. The last $MN + M$ rows of A_{ij} correspond to the homogeneous edge continuity conditions and have no more than five nonzero entries per row.

Solution

The linearized form of the flow tangency boundary condition is (Ref 5:495):

$$w/V_\infty = dc/dx - \alpha \quad (3.25)$$

Where α is the wing angle of attack, dc/dx is the local camber slope and V_∞ is the free stream velocity. This expression is substituted for each w_i in eq 3.24 where dc_i/dx is the panel slope at control point i . In matrix notation,

$$\begin{bmatrix} A_{1j} \end{bmatrix} \cdot \begin{bmatrix} \theta_j \end{bmatrix} = \begin{bmatrix} v_\infty (dc_1/dx - \alpha) \\ 0 \end{bmatrix} \quad (3.26)$$

or

$$\theta_j / v_\infty = \begin{bmatrix} A_{1j} \end{bmatrix}^{-1} \cdot \begin{bmatrix} dc_1/dx - \alpha \\ 0 \end{bmatrix} \quad (3.27)$$

Forces and Moments

Once the θ_j / v_∞ are obtained for a given α and camber slope distribution, eqs (2.3) and (2.7) can be used to calculate the vorticity strength at any point on the planform. The surface perturbation velocities in terms of local vorticity are (Ref 5:508):

$$u/v_\infty = \pm \gamma/2 \quad (3.28)$$

$$v/v_\infty = \mp \delta/2 \quad (3.29)$$

The upper sign corresponds to the upper wing surface and visa-versa.

Pressure coefficients are obtained from the perturbation velocities by either using the exact isentropic expression (Ref 3:167):

$$c_p = 2 \left[(1 + (\gamma - 1)M_\infty^2) / 2(1 - ((v_\infty + u)^2 + v^2 + w^2) / v_\infty^2) \right]^{1/(\gamma - 1)} - 1 / (\gamma M_\infty^2) \quad (3.30)$$

or the second order approximation (Ref 3:167):

$$c_p = - \left[2u/v_\infty + (1 - M_\infty^2)u^2/v_\infty^2 + (v^2 + w^2)/v_\infty^2 \right] \quad (3.31)$$

which is adequate for two-dimensional and planar flows. These coefficients are integrated along chord lines to obtain local lift and moment coefficients. The appropriate expressions are

$$C_L = (1/c) \int_{x_{LE}}^{x_{TE}} (C_{p_l} - C_{p_u}) dx \quad (3.32)$$

$$C_M = (1/c^2) \int_{x_{LE}}^{x_{TE}} (C_{p_l} - C_{p_u}) x dx \quad (3.33)$$

where the subscripts l and u refer to the lower and upper wing surfaces.

IV. Results

A FORTRAN Code "WING" was developed to analyze planform flow using the methodology discussed in Sections II and III. Most of the programming techniques used in WING were previously developed by the author and can be found in Reference 8.

Program WING was exercised for a variety of four point wings, taper ratios, and sweep angles. This section presents results for two of these wings.

Two general observations are made first. One, control point location is the major factor controlling bounded numerical oscillations of the vorticity vector as it is in many current paneling routines (ex. Refs 6 and 8). Oscillations are very common if the control point is located anywhere on the leading triangle. Fewer oscillations occur if the control point is located on the trailing triangle with $.1 \leq CY \leq .5$ and $.4 \leq CX \leq .9$. Secondly, the program shows the best results when uniform spanwise paneling is used. Non-uniform spanwise paneling tends to cause oscillations in the vorticity vector. However, non-uniform chordwise paneling seems to have little effect on solution stability. The best total C_L match (with other known solutions) occurs at approximately $CY = .15$ and $CX = .75$.

Rectangular Wing

The first case examined is a rectangular wing; $AR = 8, \alpha = 5^\circ$ and $M_\infty = .1$. The wing is modeled using 11 uniformly spaced span stations and 6 non-uniformly spaced chord stations (0., .1, .3, .6,

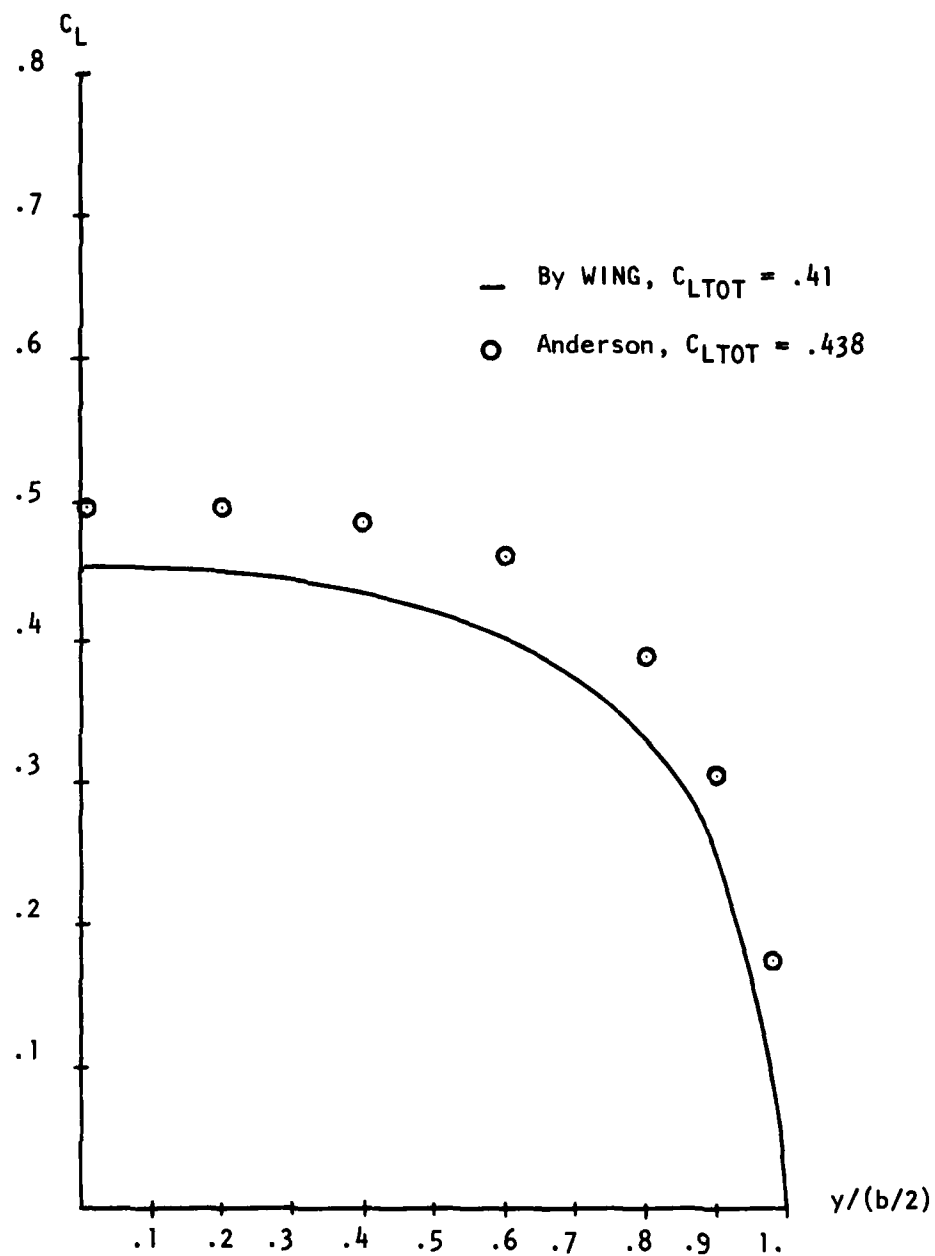


Figure 4. C_L Versus Span Station for a Rectangular Wing; $AR = 8, \alpha = 5^\circ$

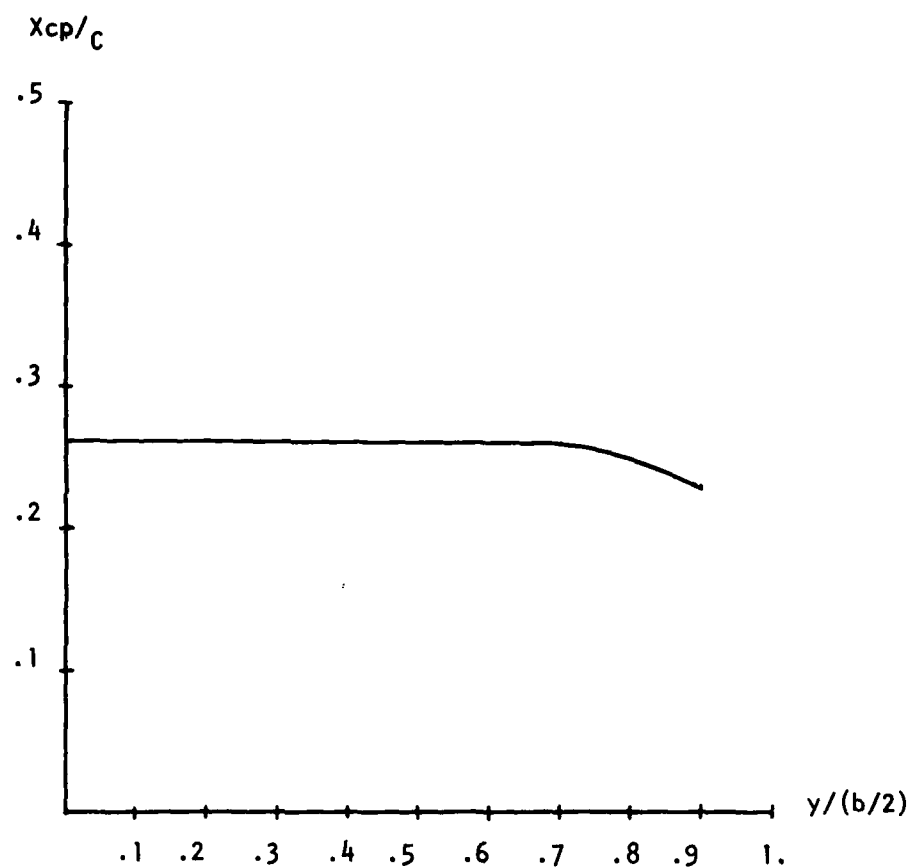


Figure 5. X_{cp}/c Versus Span Station for a Rectangular Wing; $AR = 8$, $\alpha = 5^\circ$

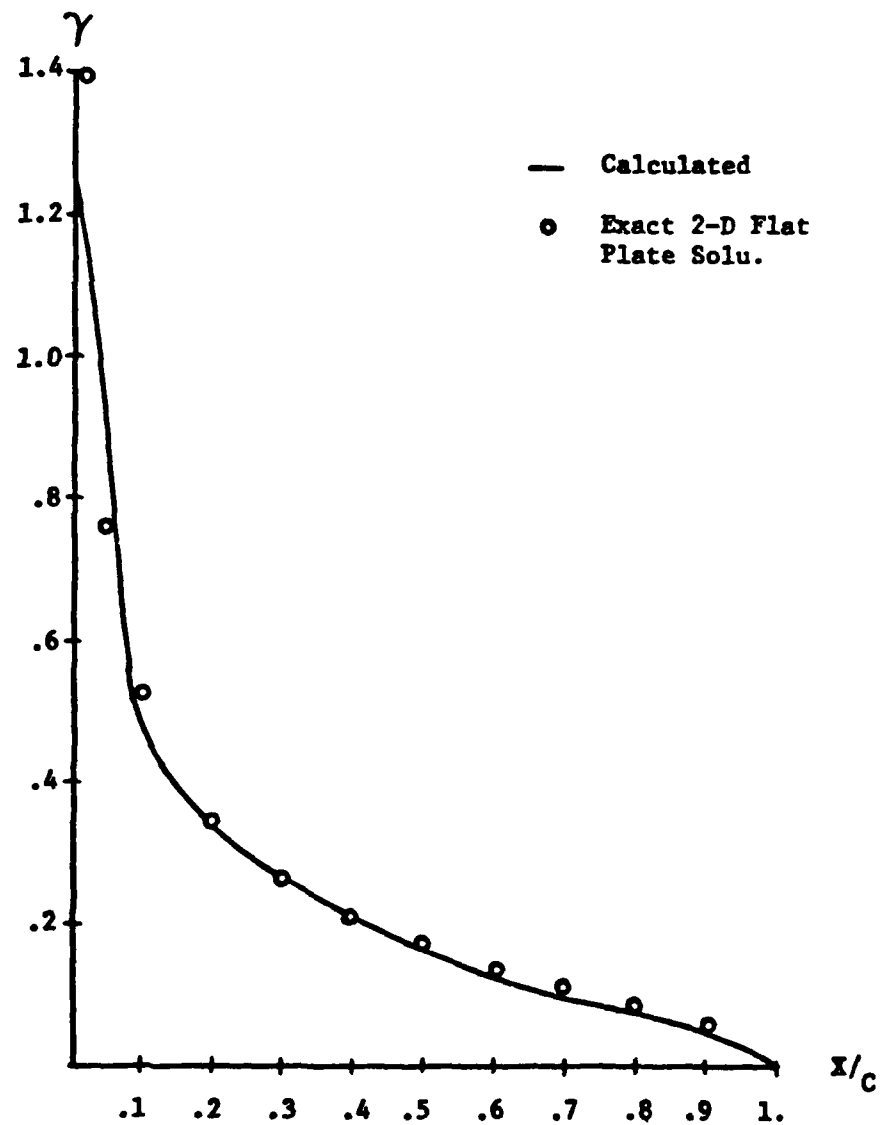


Figure 6. γ Strength Distribution at the Root Chord of a Rectangular Wing; $AR = 8$, $\alpha = 5^\circ$

.8, and 1.) which define 50 panels. Figure 4 shows the C_L distribution predicted by WING and Anderson (Ref 1:9-16). Figure 5 shows the spanwise distribution of center of pressure. The x_{cp} stays close to the classical 25% chord location except in the outboard region where it travels forward as expected.

Figure 6 is the γ strength at the root chord. The calculated solution compares favorably with the exact 2-D flat plate solution (Ref 5:515):

$$\gamma(x) = 2 \alpha (c - x) / (cx - x^2) \quad (5.1)$$

where c is the chord length and α is measured in radians.

Swept Wing

The second case examined is a swept untapered wing; $AR = 4.5$, $\Lambda = 40^\circ$, $\alpha = 5^\circ$, and $M_\infty = .1$. The wing modeling is the same as the rectangular wing. Figure 7 shows the C_L distribution predicted by WING and by wind tunnel tests (Ref 4:92). Figure 8 shows the x center of pressure versus span station. Again, good agreement is obtained for both the C_L distribution and x_{cp} travel.

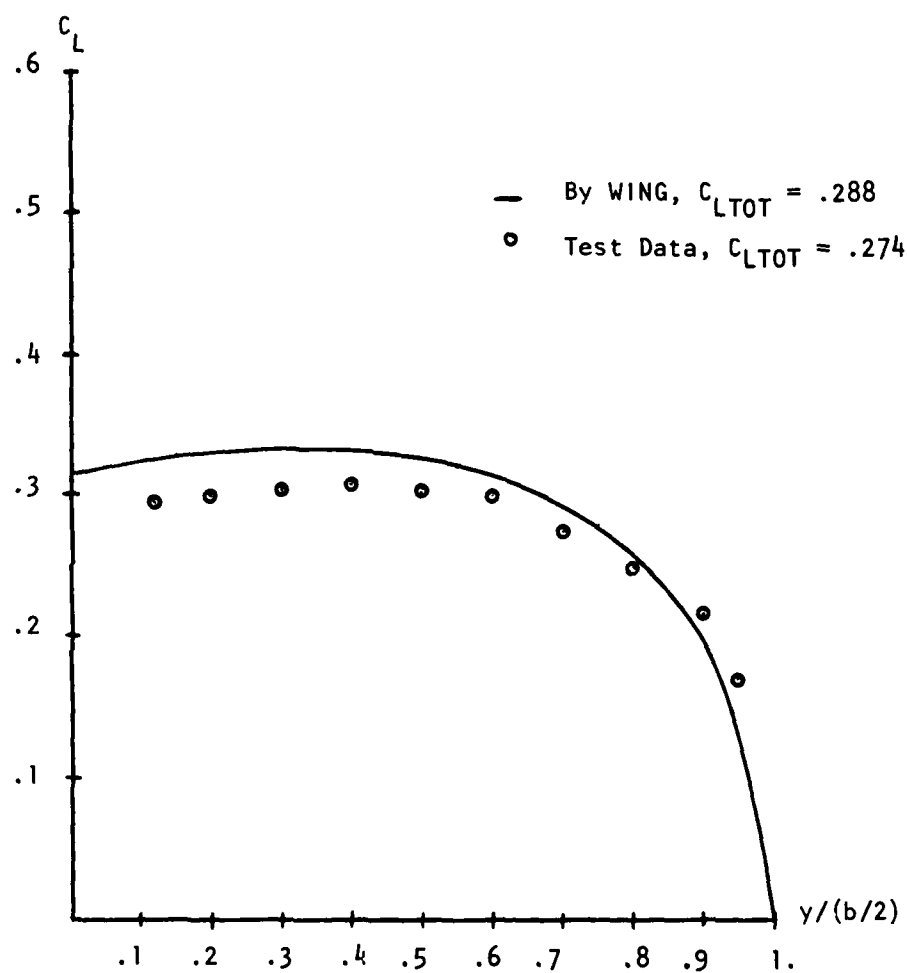


Figure 7. C_L Versus Span Station for a Sweptback Untapered Wing; $AR = 4.5$, $\Lambda = 40^\circ$, $\alpha = 5^\circ$

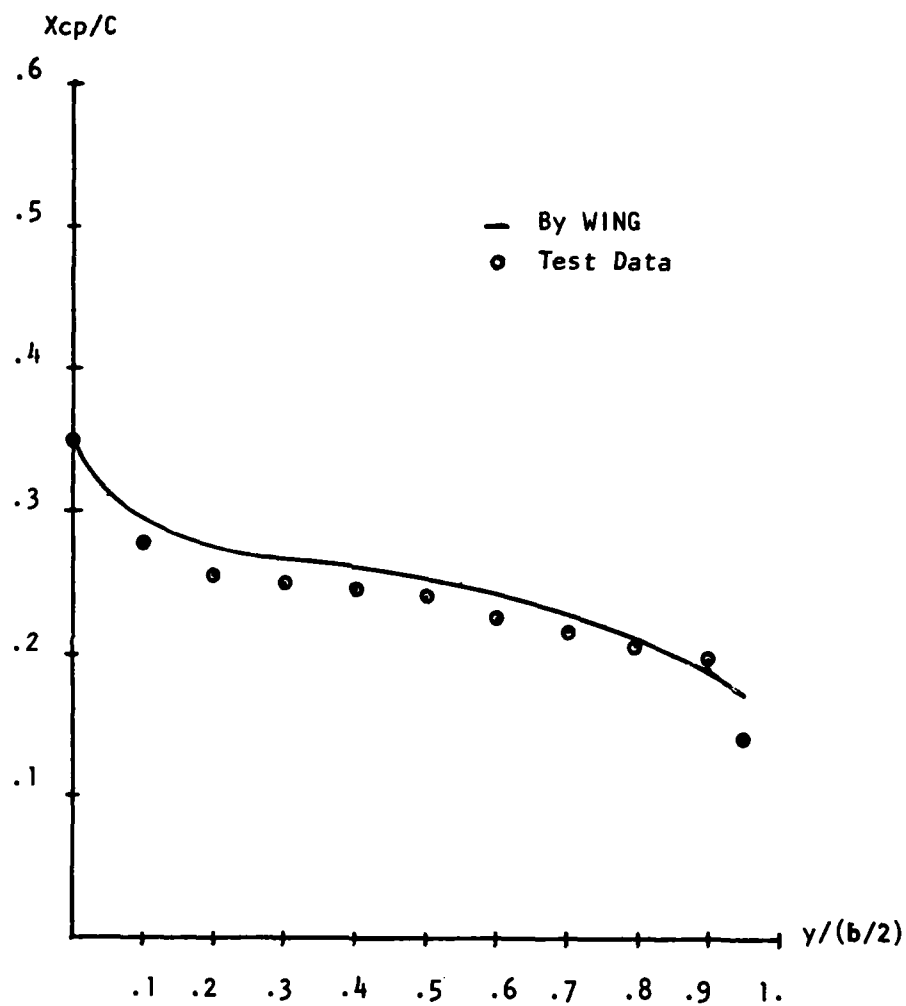


Figure 8. X_{cp}/C Versus Span Station for a Sweptback Untapered Wing; $AR = 4.5$, $\Lambda = 40^\circ$, $\alpha = 5^\circ$

V. Conclusions and Recommendations

Conclusions

A paneling technique which allows the vorticity vector to change direction has been demonstrated. The proper choice of control point (see section IV) will guarantee a solution free of numerical oscillations in the vorticity vector. This method has been implemented on a computer and introduces no new complexities to an experienced programmer. Existing mesh generators and other aerodynamic modules were incorporated into this technique (Ref 8). Computer run times are of the same order as programs incorporating "fixed direction" vorticity panels and no problems involving extensive "run times" were encountered.

The method gives satisfactory aerodynamic results for the cases examined. However, as in other paneling methods, the results are control point sensitive and some "curve fitting" is involved to find the control point location that best matches existing data or solutions. Also, the best "fits" don't shown any appreciable improvement over existing paneling methods such as the constant strength vorticity panel program described in reference 8.

Recommendations

The following ideas are suggested for further study or improvement of the method:

- a. The method should be tested for cranked wings.
- b. The panel should be oriented in space to allow method assessment for three dimensional flow situations.

APPENDIX A

Evaluation of the Panel Integrals

The methodology for evaluating the integrals $I_i^{L,T}$ of section 2 is presented here.

Consider the semi-infinite region shown in Figure 9. This strip is bound by the lines $y = y_0$, $y = y_1$, and the line segment connecting (x_0, y_0) to (x_1, y_1) . The equation for the line segment is:

$$y = Mx + b \quad (A.1)$$

where

$$M = ((y_1 - y_0)/(x_1 - x_0)) \quad (A.2)$$

and

$$b = y_0 - x_0 M \quad (A.3)$$

Define the following improper integrals on the semi-infinite strip

$$F_i = \lim_{L \rightarrow \infty} \int_{y_0}^{y_1} \int_{(y-b)/M}^L f_i(x, y) dx dy \quad (i = 1, \dots, 5) \quad (A.4)$$

where

$$f_1(x, y) = x/(x^2 + y^2)^{3/2} \quad (A.5)$$

$$f_2(x, y) = x^2/(x^2 + y^2)^{3/2} \quad (A.6)$$

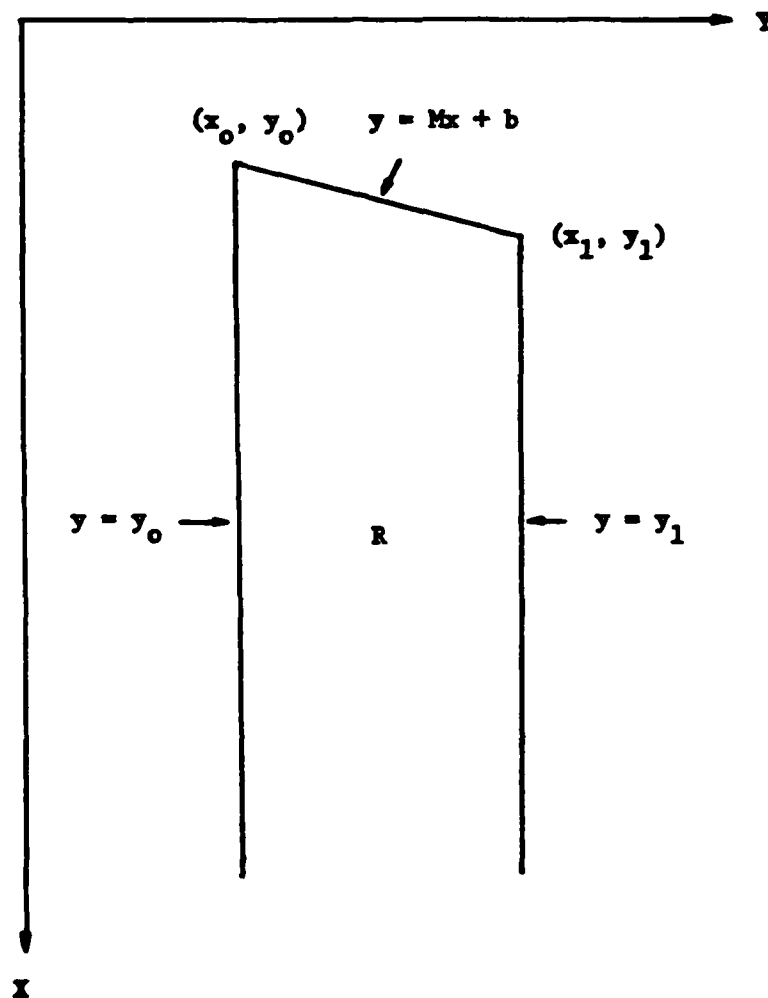


Figure 9. Semi-Infinite Strip R Used In Integral Evaluation

$$f_3(x, y) = xy/(x^2 + y^2)^{3/2} \quad (A.7)$$

$$f_4(x, y) = y/(x^2 + y^2)^{3/2} \quad (A.8)$$

and

$$f_5(x, y) = y^2/(x^2 + y^2)^{3/2} \quad (A.9)$$

To illustrate the methodology used in evaluating the integrals (A.4), consider

$$F_5 = \lim_{L \rightarrow \infty} \int_{y_0}^{y_1} \int_{(y-b)/M}^L [y^2/(x^2 + y^2)^{3/2}] dx dy \quad (A.10)$$

By Pierce's integral tables (Ref 7),

$$F_5 = \lim_{L \rightarrow \infty} \int_{y_0}^{y_1} [y^2 x / (y^2 \sqrt{x^2 + y^2})] \Big|_{(y-b)/M}^L dy = \quad (A.11)$$

$$\lim_{L \rightarrow \infty} \int_{y_0}^{y_1} L dy / \sqrt{L^2 + y^2} - \int_{y_0}^{y_1} ((y-b)/M) dy / \sqrt{((y-b)/M)^2 + y^2} \quad (A.12)$$

Substituting

$$z = (y-b)/M \quad (A.13)$$

and

$$dy = M dz \quad (A.14)$$

into the rightmost integral of (A.12) yields:

$$F_5 = \lim_{L \rightarrow \infty} \int_{y_0}^{y_1} (L dy / \sqrt{L^2 + y^2}) - M \int_{x_0}^{x_1} \frac{z dz}{\sqrt{z^2 + (Mx + b)^2}} \quad (A.15)$$

The integrals (A.15) can be evaluated using Ref. 7. One obtains, after some algebraic manipulation,

$$\begin{aligned} F_5 = \lim_{L \rightarrow \infty} L \ln[(y_1 + \sqrt{y_1^2 + L^2}) / (y_0 + \sqrt{y_0^2 + L^2})] + \\ [bM^2 / (1 + M^2)^{3/2}] \ln[(\sqrt{x_1^2 + y_1^2} + ((x_1 + My_1) / \\ \sqrt{1 + M^2})) / (\sqrt{x_0^2 + y_0^2} + ((x_0 + My_0) / \sqrt{1 + M^2}))] + \\ [M / (1 + M^2)] (\sqrt{x_0^2 + y_0^2} - \sqrt{x_1^2 + y_1^2}) \end{aligned} \quad (A.16)$$

recalling

$$y_0 = Mx_0 + b \quad (A.17)$$

and

$$y_1 = Mx_1 + b \quad (A.18)$$

Notice the limit

$$\lim_{L \rightarrow \infty} L \ln[(y_1 + \sqrt{y_1^2 + L^2}) / (y_0 + \sqrt{y_0^2 + L^2})] \quad (A.19)$$

is not a function of x_0 or x_1 which leads to the following observation. If the integral F_5 is evaluated on any other semi-infinite strip bounded by the lines $y = y_0$ and $y = y_1$, the limit (A.19) is invariant. Evaluating the integral F_5 using any other line segment connecting $y = y_0$ to $y = y_1$ and formulating the difference between this result and (A.16) leads to cancellation of the limit (A.19).

The other four integrals, F_1 through F_4 , can be evaluated by a similar procedure using Ref 7. Each integral has a limit term given by:

$$(F_1) \quad \lim_{L \rightarrow \infty} \ln[(y_0 + \sqrt{y_0^2 + L^2}) / (y_1 + \sqrt{y_1^2 + L^2})] \quad (A.20)$$

$$(F_2) \quad \lim_{L \rightarrow \infty} [y_1 \ln(\sqrt{L^2 + y_1^2} + L) - y_0 \ln(\sqrt{L^2 + y_0^2} + L)] \quad (A.21)$$

$$(F_3) \quad \lim_{L \rightarrow \infty} [\sqrt{L^2 + y_0^2} - \sqrt{L^2 + y_1^2}] \quad (A.22)$$

$$(F_4) \quad \lim_{L \rightarrow \infty} \ln[(L + \sqrt{L^2 + y_0^2}) / (L + \sqrt{L^2 + y_1^2})] \quad (A.23)$$

These terms cancel upon the formulation of integral differences.

Retaining the finite terms from each of the integral evaluations, we can define "Strip Functions" S_i for the functions f_i and the points (x_0, y_0) and (x_1, y_1) by

$$S_1[(x_0, y_0), (x_1, y_1)] = (M/\sqrt{1+M^2})C \quad (A.24)$$

$$\begin{aligned}
s_2[(x_0, y_0), (x_1, y_1)] &= y_0 \ln[\sqrt{x_0^2 + y_0^2} + x_0] - \\
& y_1 \ln[\sqrt{x_1^2 + y_1^2} + x_1] + (M/(1 + M^2))H + \\
& [b/(1 + M^2)^{3/2}]G
\end{aligned}
\tag{A.25}$$

$$\begin{aligned}
s_3[(x_0, y_0), (x_1, y_1)] &= (M^2/(1 + M^2))H + \\
& [bM/(1 + M^2)^{3/2}]G
\end{aligned}
\tag{A.26}$$

$$\begin{aligned}
s_4[(x_0, y_0), (x_1, y_1)] &= \ln[(x_1 + \sqrt{x_1^2 + y_1^2})/ \\
& (x_0 + \sqrt{x_0^2 + y_0^2})] - G/\sqrt{1 + M^2}
\end{aligned}
\tag{A.27}$$

$$\begin{aligned}
s_5[(x_0, y_0), (x_1, y_1)] &= [bM^2/(1 + M^2)^{3/2}]G - \\
& (M/(1 + M^2))H
\end{aligned}
\tag{A.28}$$

where

$$\begin{aligned}
G &= \ln[(\sqrt{x_1^2 + y_1^2} + ((x_1 + My_1)/\sqrt{1 + M^2}))/ \\
& (\sqrt{x_0^2 + y_0^2} + ((x_0 + My_0)/\sqrt{1 + M^2}))]
\end{aligned}
\tag{A.29}$$

and

$$H = \sqrt{x_1^2 + y_1^2} - \sqrt{x_0^2 + y_0^2}
\tag{A.30}$$

Examining Figure 1, it is obvious that each of the panel integrals (2.30) through (2.34) can be obtained by formulating the difference of

two corresponding strip functions. This leads to the following

fundamental results:

$$I_1^L = s_1[(x_1, y_1), (x_3, y_2)] - s_1[(x_1, y_1), (x_4, y_2)] \quad (A.31)$$

$$I_1^T = s_1[(x_1, y_1), (x_4, y_2)] - s_1[(x_2, y_1), (x_4, y_2)] \quad (A.32)$$

where i ranges from 1 to 5.

APPENDIX B

Simple Wake Model

The Kutta condition (Ref 5:390-399) implies

$$\vec{\omega}(x, y) = \delta(x, y) \vec{i} \quad (\text{B.1})$$

for all points on the wing trailing edge. Let vortex filaments emanate from corners 2 and 4 of a trailing edge panel and extend to infinity (see Figure 10). By Helmholtz's theorems, these filaments will retain the strengths δ_2 and δ_4 indefinitely. Now assume that the strength of the wake region between the two filaments is given by:

$$\delta(x, y) = (My + b) \vec{i} \quad (\text{B.2})$$

where

$$M = (\delta_4 - \delta_2) / (y_2 - y_1) \quad (\text{B.3})$$

$$b = \delta_2 - y_1 [(\delta_4 - \delta_2) / (y_2 - y_1)] \quad (\text{B.4})$$

Applying the Biot-Savart Law (Section 11), the effect of the wake region upon the induced velocity at a control point located at the origin of the coordinate system is

$$\begin{aligned} 4\pi W = & -M S_5[(x_2, y_1), (x_4, y_2)] \\ & -b S_4[(x_2, y_1), (x_4, y_2)] \end{aligned} \quad (\text{B.5})$$

The limit terms (A.23) and (A.19) for the "Strip Functions" S_4 and S_5 must now be evaluated and

$$(S_4) \lim_{L \rightarrow \infty} \ln [(L + \sqrt{L^2 + y_1^2}) / (L + \sqrt{L^2 + y_2^2})] = 0 \quad (\text{B.6})$$

$$(S_5) \lim_{L \rightarrow \infty} L \ln [(y_2 + \sqrt{y_2^2 + L}) / (y_1 + \sqrt{y_1^2 + L})] = y_2 - y_1 \quad (\text{B.7})$$

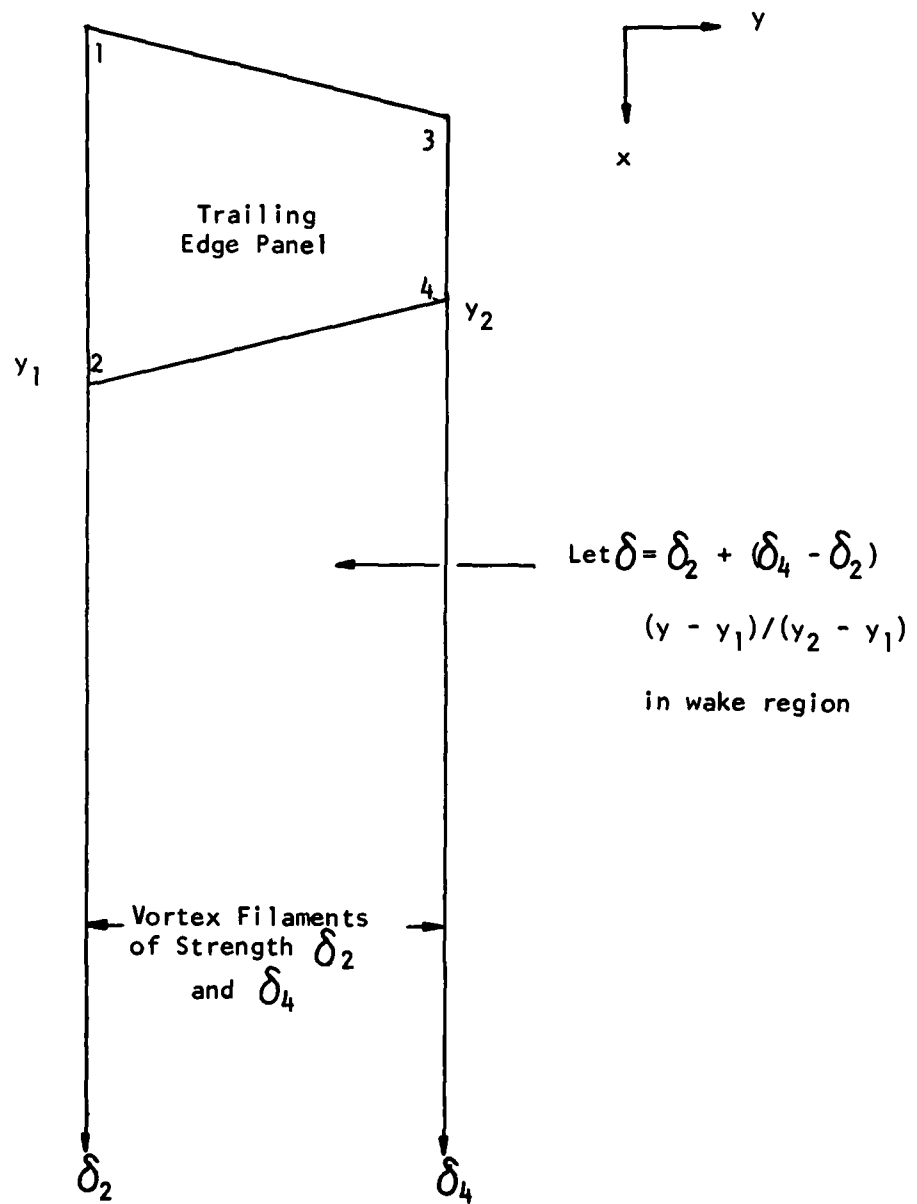


Figure 10. Wake Model

Collecting coefficients of δ_2 and δ_4 , we obtain

$$\begin{aligned} 4\pi W = & [(s_5 - \gamma_2 s_4)/(\gamma_2 - \gamma_1)] \delta_2 \\ & + [(\gamma_1 s_4 - s_5)/(\gamma_2 - \gamma_1)] \delta_4 \end{aligned} \quad (B.8)$$

which is the induced velocity at a point due to a wake region emanating behind an arbitrary trailing edge panel.

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